

## CFD - Lecture 9

- Odds & ends,

- quiz next week (informal, nearly direct from class notes)
- final projects

- groups are fine

- make an appointment to discuss

In upcoming HW, include an email

My group is: (names)

My project title is: ( )

My project will study/produce: (deliverables)

In my 8 min presentation, I will show ( )

### Today

- Recall laminar channel flow
- What happens when  $Re \uparrow$  ?
- Some videos
- An overview of turbulence modelling
- Turbulent flow over a sphere

Turbulence is an extremely rich topic, but to solve practical problems, need a rough understanding of how to get a decent ~~model~~ tractable model.

When I meet god, I am going to ask two questions: why relativity and why turbulence? I really believe he will have an answer for the first a  
Heisenberg

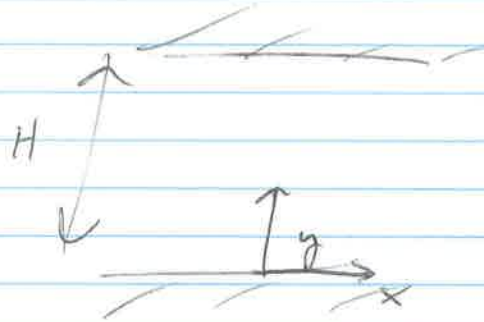
## Poiseuille flow

Assume  $u = u(y)$  on

$$\vec{u} = \langle u(y), 0, 0 \rangle$$

$$p = p(x) = \text{const.}$$

$$\nabla \cdot \vec{u} = \partial_x u(y) = 0 \quad \checkmark$$



$$\cancel{\partial_x u} + u \cdot \nabla u = -\nabla p + \nu \nabla^2 u$$

$$u(0) = u(H) = 0$$

$$\cancel{u \partial_x u} + \nu \cancel{\partial_y^2 u} = -\partial_x p + \nu (\cancel{\partial_x^2 u} + \partial_y^2 u)$$

$$\partial_y^2 u = \partial_x p$$

$$\nu \frac{d^2 u}{dy^2} = \frac{\partial p}{\partial x}$$

$$\nu \frac{du}{dy} + C_1 u = y \frac{\partial p}{\partial x} + C_1$$

$$\nu u(y) = \frac{1}{2} y^2 \frac{\partial p}{\partial x} + C_1 y + C_2$$

$$0 = u(0) = C_2$$

$$0 = u(H) = \frac{1}{2} H^2 \frac{\partial p}{\partial x} + C_1 H \rightarrow C_1 = -\frac{1}{2} H \frac{\partial p}{\partial x}$$

$$\nu u(y) = \frac{1}{2} \frac{\partial p}{\partial x} (y^2 - Hy)$$

$$u(y) = \frac{1}{2\nu} \frac{\partial p}{\partial x} y(y-H)$$

$$Q = \int_{\text{inlet}} u \cdot n \, dA = - \int_0^H u(y) \, dy = -\frac{H^3}{6}$$
$$= -\frac{1}{2\nu} \frac{\partial p}{\partial x} \int_0^H y(y-H) \, dy$$

$$Q = \frac{H^3}{12\nu} \frac{\partial p}{\partial x}$$

## Statistical treatment of turbulence

- Seen from videos a wide range of length scales

$l_{char}^{big} \rightarrow$  geometry dependent  
 $l_{char}^{small} = ?$

~~To estimate scale of smallest eddies, consider the viscous length scale~~

- At some point viscous forces dominate

$$F \sim \nu \nabla^2 u \sim \frac{\nu U_{char}^{small}}{l_{char}^{small}}$$

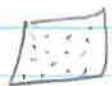


- Idea • turbulence is fundamentally unsteady  
• separate velocity into an average and fluctuating component

$$u = \bar{u} + u'$$

- Molecular dynamics analogue: For molecular fluctuations, the bulk flow is governed by ensemble average

$$\bar{u}_{molecular} \sim \frac{1}{N} \sum u_i$$



explain ensemble average



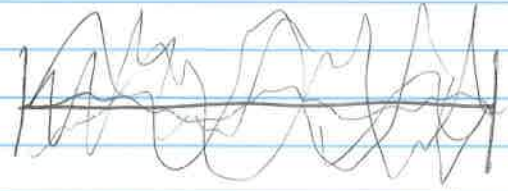
- Ergodic hypothesis  
- can exchange ensemble average with time average

- So if we took a bunch of snapshots of the channel flow problem, and average them together, we obtain a mean profile  $\bar{u}$ ,

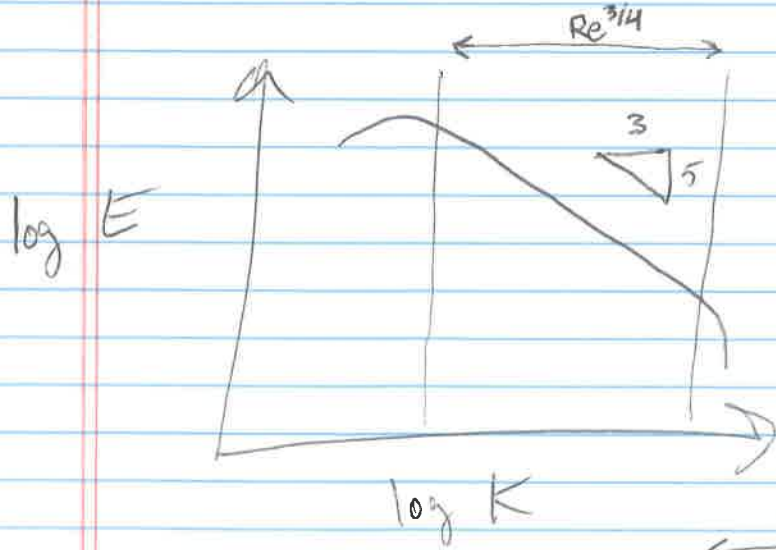


and obtain a collection of "random" variables  $u' = u - \bar{u}$

- Why "random"?
- How does  $\bar{u}$  compare to  $u \sim y(H-y)$ ?

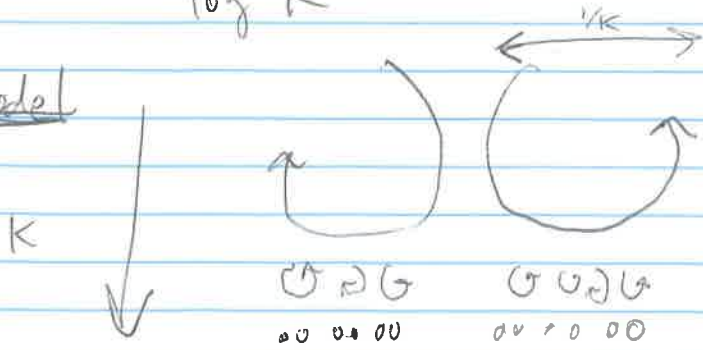


- Study the structure of these fluctuations by considering the energy contained in each mode in its Fourier spectrum



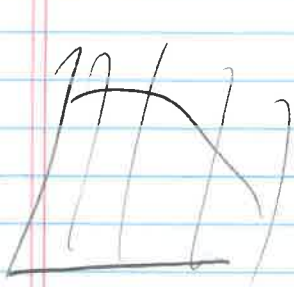
- $E \sim u' u'^2$
- $K \sim 1/\text{eddy size}$
- lengthscale ratio  $Re^{3/4}$   
 → in 3D we need  $Re^{9/4}$  scales

Model

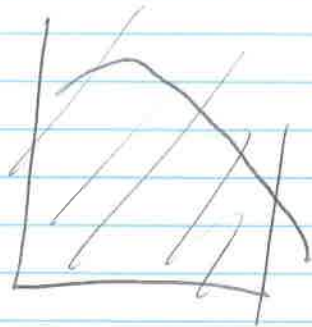


Re in nature	
Fish (small slow)	1
Blood flow	10-100
MLB pitch	$2 \times 10^5$
Fish (p-stest)	$10^6$
Whale	$10^8$
Big ship	$10^7$

- Need to model



DNS



LES



RANS

Goal = resolve  $\bar{u}$ , model  $u'$

Define averaging operator as  $\overline{u\bar{v}} = \bar{u}\bar{v}$   
 $\overline{u'} = 0$  and assume commutes w/ derivative

Stick  $u = \bar{u} + u'$  into N-S

$$\rho \frac{\partial u}{\partial t} + u \cdot \nabla u = -\nabla p + \nu \nabla^2 u$$

Mom.  $\rho \frac{\partial (\bar{u} + u')}{\partial t} + (\bar{u} + u') \cdot \nabla (\bar{u} + u') = -\nabla \bar{p} + p' + \nu \nabla^2 \bar{u} + u'$

Mass:  $\nabla \cdot (\bar{u} + u') = 0$

Take average of mass

$$0 = \overline{\nabla \cdot (\bar{u} + u')} = \nabla \cdot \bar{u} + \overline{\nabla \cdot u'} = \boxed{\nabla \cdot \bar{u} = 0}$$

For mom. Similarly, all the linear terms' fluctuating part drops out, except

$$(\bar{u} + u') \cdot \nabla (\bar{u} + u') = \bar{u} \cdot \nabla \bar{u} + \bar{u} \cdot \nabla u' + u' \cdot \nabla \bar{u} + u' \cdot \nabla u'$$

Take average

$$= \overline{\bar{u} \cdot \nabla \bar{u}} + \overline{\bar{u} \cdot \nabla u'} + \overline{u' \cdot \nabla \bar{u}} + \overline{u' \cdot \nabla u'}$$

$$= \bar{u} \cdot \nabla \bar{u} + \overline{u' \cdot \nabla u'} \leftarrow \text{Reynolds stresses}$$

And we get Reynolds-Averaged N.S eqns  
(RANS)

$$\begin{cases} \rho_t \bar{u} + \bar{u} \cdot \nabla \bar{u} = -\nabla \bar{p} + \nu \nabla^2 \bar{u} + \overline{u' \cdot \nabla u'} \\ \nabla \cdot \bar{u} = 0 \end{cases}$$

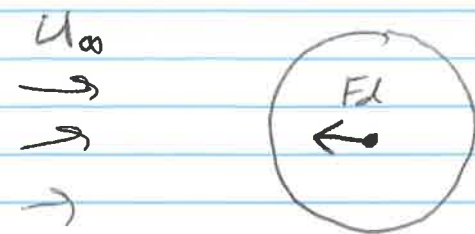
Same as N-S  
but with new  
term

Assignment: (due 5/1)

The drag force can be expressed as

$$F_d = \frac{1}{2} C_D \rho U_{\infty}^2 A$$

$\uparrow$  Drag coefficient  
 $\uparrow$  density  
 $\uparrow$  Frontal Cross-sectional area



- ① Set up 3D sphere geometry from Holtzmann-CFO website
- ② Confirm that you can match drag for low-Re case
- ③ Add K-ε turbulence model (we'll cover this next week) and reproduce the graph of  $C_D$  vs  $Re$  for  $Re \in [10^0, 10^1, 10^2, 10^3, 10^4, 10^5, 10^6]$