

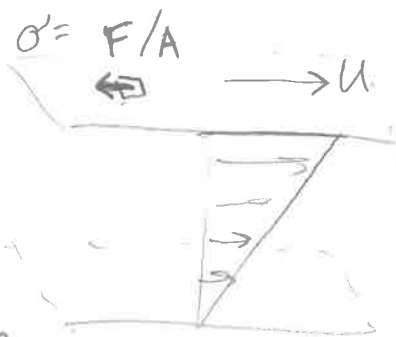
CFD - Lecture 8

- Incompressible Navier-Stokes equations
- Non-dimensionalization & the Reynolds number
- Building a mesh
- HW workshop

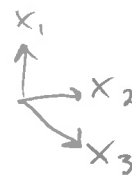
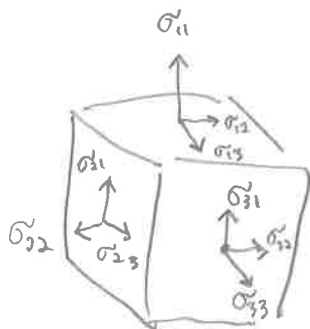
- Today we'll present methods for solving the incompressible Navier-Stokes \rightarrow first, what are they?

Viscous flow

For a Newtonian fluid we assume that our fluid stresses are linearly proportional to the local strain rate of the flow



- For a unit box, we can consider the stresses coming from 3 directional components at each face



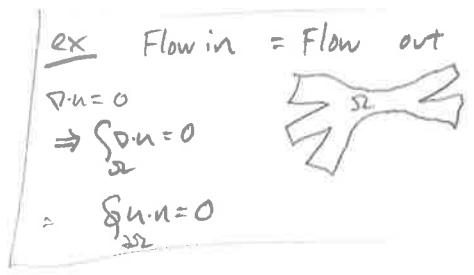
$$\sigma_{ij} = -p \delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

- Pushing this through the usual momentum conservation argument, we obtain

$$\partial_t \rho u + \nabla \cdot \rho u^2 = -\nabla p + \nabla \cdot \mu (\nabla u + \nabla u^T)$$

- For slow-moving fluids $Ma = \frac{u}{c} \ll 1$ we can assume that density is constant

Mass \rightarrow ~~$\partial_t \rho$~~ + $\nabla \cdot \rho u = 0$
 $\rho \nabla \cdot u = 0$



$$\boxed{\nabla \cdot u = 0}$$

also $\rho = \text{const.}$
 converse

- Rather than coupling pressure, EOS, conservation together, we can instead solve

$$\begin{cases} \partial_t \rho u + \nabla \cdot \rho u^2 = -\nabla p + \nabla \cdot \mu (\nabla u + \nabla u^T) \\ \nabla \cdot u = 0 \end{cases}$$

ρ, μ given, 2 equations + 2 unknowns (u, p)

With some arithmetic this can be written as

$$\begin{cases} \partial_t u + u \cdot \nabla u = -\frac{1}{\rho} \nabla p + \frac{\mu}{\rho} \nabla^2 u \\ \nabla \cdot u = 0 \end{cases}$$

This can be further simplified

Kinetic viscosity $\nu = \frac{\mu}{\rho}$

let $p^* = \frac{p}{\rho}$

Navier - Stokes equations.

$$\begin{cases} \partial_t u + u \cdot \nabla u = -\nabla p^* + \nu \nabla^2 u \\ \nabla \cdot u = 0 \end{cases}$$

customary to drop
the $p^* \rightarrow p$

How to understand \rightarrow advection vs diffusion

\rightarrow pressure acting as Lagrange mult.

Non-dimensionalization

Let u^*, l^* be characteristic length + timescales

$$\bar{x} = \frac{x}{l^*} \quad \bar{t} = \frac{t}{l^* u^*} \quad \bar{u} = \frac{u}{u^*} \quad \bar{p} = \frac{p l^*}{\rho u^{*2}}$$

$$\partial_t u = \frac{d\bar{t}}{dt} \frac{\partial u}{\partial \bar{t}} = \frac{dt}{d\bar{t}} \frac{du}{d\bar{u}} \frac{\partial \bar{u}}{\partial \bar{t}} = \frac{1}{l^* u^*} u^* \frac{\partial \bar{u}}{\partial \bar{t}} = \frac{1}{l^*} \frac{\partial \bar{u}}{\partial \bar{t}}$$

Continuing with this term by term we obtain

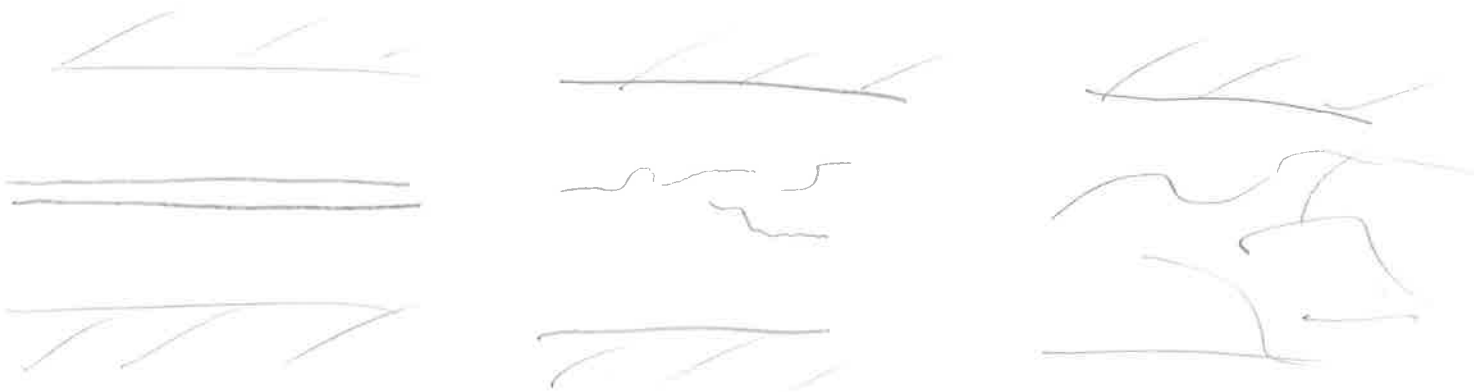
where $\nabla = (\partial_{x_1}, \partial_{x_2}, \partial_{x_3})$

$$\partial_t \bar{u} + \bar{u} \cdot \nabla \bar{u} = -\nabla \bar{p} + \frac{1}{Re} \nabla^2 \bar{u}$$

where $Re = \frac{U^* l^*}{\nu}$ is the Reynolds Number

Two limits $Re \downarrow 0$ or $Re \rightarrow \infty$

Original experiment by Reynolds



Today we'll do a similar experiment...

First - how to solve NS?

- Projection method (predictor corrector)

① Semi-discretize in time

$$\frac{u^{n+1} - u^n}{\Delta t} + u^n \cdot \nabla u^{n+1} = -\nabla p^{n+1} + \nu \nabla^2 u^{n+1}$$

$$\nabla \cdot u^{n+1} = 0$$

- What does this matrix look like?

② Split into non-div-free momentum

$$\frac{u^* - u^n}{\Delta t} + u^n \cdot \nabla u^* = \nu \nabla^2 u^*$$

- note $\nabla \cdot u^* \neq 0$

③ Add a correction such that $\nabla \cdot u^{n+1} = 0$

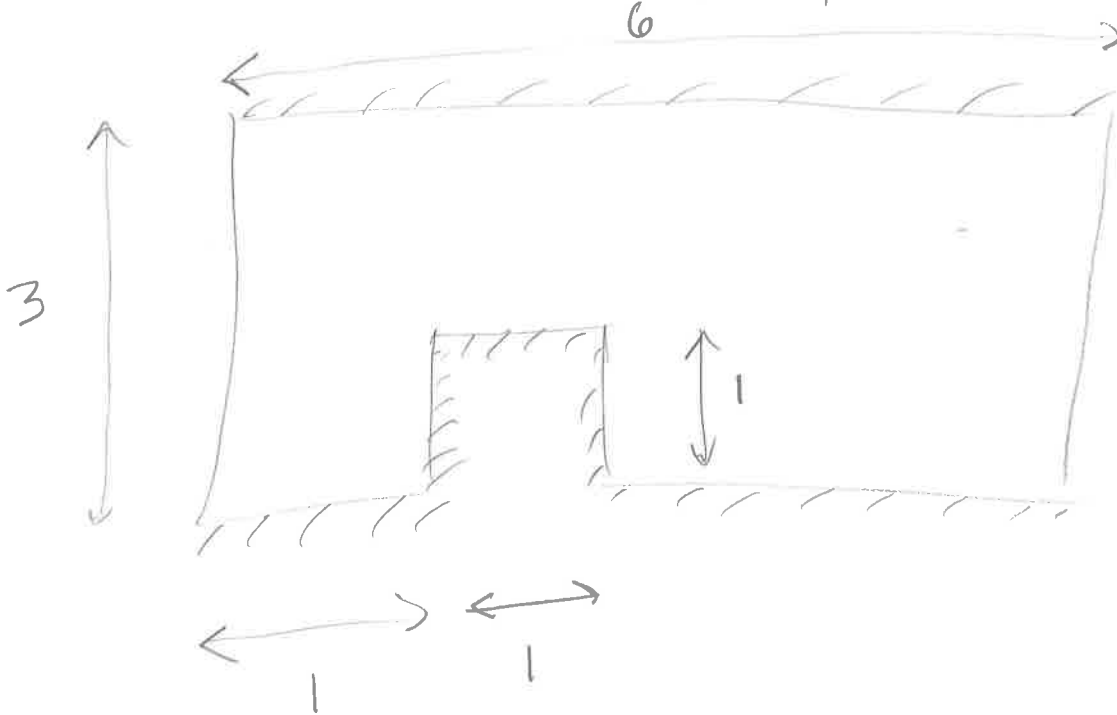
$$\frac{u^{n+1} - u^*}{\Delta t} = -\nabla p^{n+1}$$

$$\nabla \cdot \left(\frac{u^{n+1} - u^*}{\Delta t} \right) = -\nabla^2 p^{n+1} \Rightarrow \nabla^2 p^{n+1} = \frac{\nabla \cdot u^*}{\Delta t}$$

- We know how to do all of these things
in OpenFOAM...

HW 6

- Implement projection method in OpenFOAM
- Simulate the following problem:



Apply the following BC

velocity

- inlet - uniform $u = \langle 1, 0 \rangle$
- outlet - $\nabla u \cdot \hat{n} = 0$
- walls - no-slip $u = \langle 0, 0 \rangle$

pressure

- outlet - $p = \text{arbitrary const.}$
- everywhere else - $\partial_n p = 0$

Run a simulation to $t_{\text{final}} = 7$ for

$Re = [0.1, 1, 10, 100, 1000]$ by varying ν .